

## DEVELOPMENT OF A LASER-GUIDED DEEP-HOLE MEASUREMENT SYSTEM: USAGE OF A LONG MEASUREMENT BAR

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**Abstract**-This paper presents measurement methods of deep holes by using a measurement unit attached to the end of a long cylindrical measurement bar. The system consists of a measurement unit for scanning hole walls, a laser interferometer for detecting the topography of hole walls and an optical device for detecting the attitude of the measurement unit. The measurement unit at the end of the measurement bar is positioned along a hole's centerline and is supported by a pair of skids. A computational analysis showed that a 3 m deep-hole with a diameter of 63mm can be measured by this measurement system.

**Keywords:** Deep-Hole, Measurement, Accuracy, Laser Application, Probe

### 1. INTRODUCTION

It is essential to accurately measure the diameter, roundness, cylindricity, and straightness of a deep hole for applications such as the rotation shafts of jet engines, generators and high-speed trains; the cylinder used in plastic injection molding; and the cylindrical liners of ship engines. Existing systems have drawbacks in precisely measuring holes with large-length-to diameter ratios, in which multiple measurement devices are required. In order to accurately evaluate the parameters of such deep holes using a single device, a laser-guided deep-hole evaluation probe was developed (Fig.1) [1]. The attitude (position and inclination) of the probe is controlled so that it stays on the measurement axis (Fig.2). A measurement unit rotates and its stylus scans the hole wall. The movement of the stylus is detected by a laser interferometer located in front of the probe.

It is difficult to measure the accuracy of deep holes of the order of a few meters with diameters varying of the order of a few millimeters, such as the rotating shaft holes of jet engines and high-speed trains. In these cases, multiple measurement devices are required to separately measure hole accuracy.

Figure 3 shows the relationships between a measurement bar's length and its deflection in a deep hole. One condition is a cantilever with a fixed end and a free end. Figure 3(a) is the case in which the rigidity of the measurement bar is maintained. Many measurement devices that

operate under this condition are available in the market. Figure 3(b) shows the case for which measurement is possible if the end of the measurement bar is supported. Figure 3(c) is the case in which the rigidity of the measurement bar is low and measurement without actuators is impossible. In this case, a measurement system as shown in Figs. 1 and 2 is necessary.

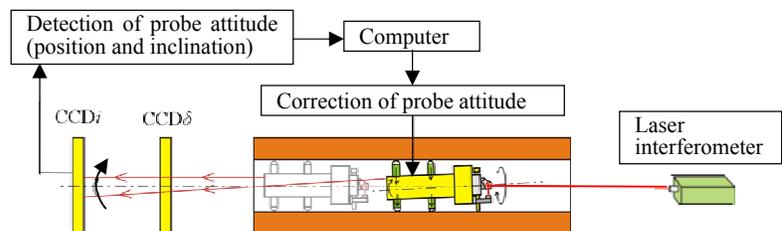
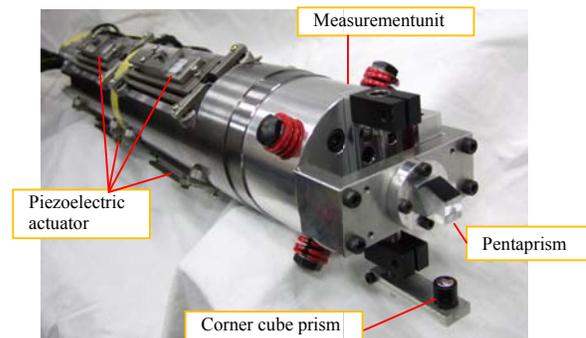


Fig.2: Structure of a laser-guided deep-hole measurement probe

In this paper, it is shown theoretically that hole accuracy can be measured when the measurement bar is a cantilever with a supported end. Further, a method for simulating measurement of a 3 m deep hole using a deep-hole measurement device with a small transverse length of machine table is shown. This method is very useful because a large measurement machine with a length of double the hole depth is necessary for evaluating the accuracy of holes with lengths of a few to several meters and is difficult to facilitate in laboratory.

## 2. DESIGN OF THE MEASUREMENT SYSTEM

### 2.1 Deep-Hole Measurement System

Figure 4 shows the deep-hole measurement system, which uses a hollow shaft as the long measurement bar [2]. A conventional lathe is used, with one end of the measurement bar fixed by the collet chuck and the other end supported by a pair of skids [10] behind the measurement unit [1] [3]. Workpiece is fixed on a machine table. The hole wall is scanned spirally by rotating the measurement unit and feeding the workpiece along the measurement unit, which is rotated by a stepping motor [7]. Up and down movement of a stylus is detected by a laser interferometer [4], which

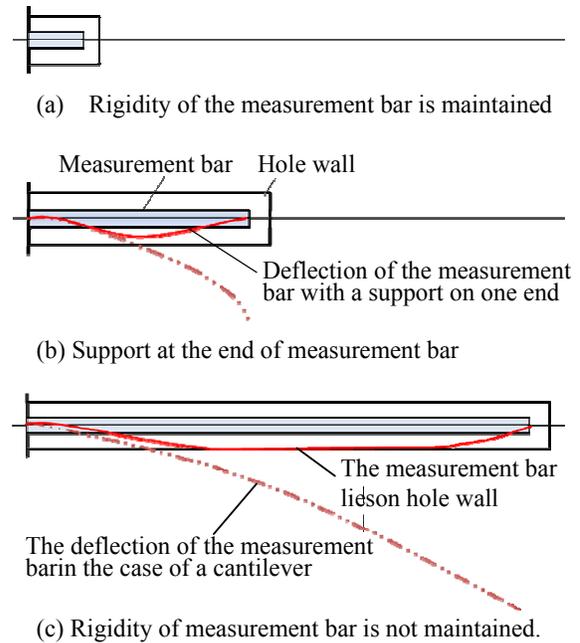


Fig.3: Deflections of measurement bars of varying lengths in deep holes with support at one end.

Therefore, the rotational deviation of the laser

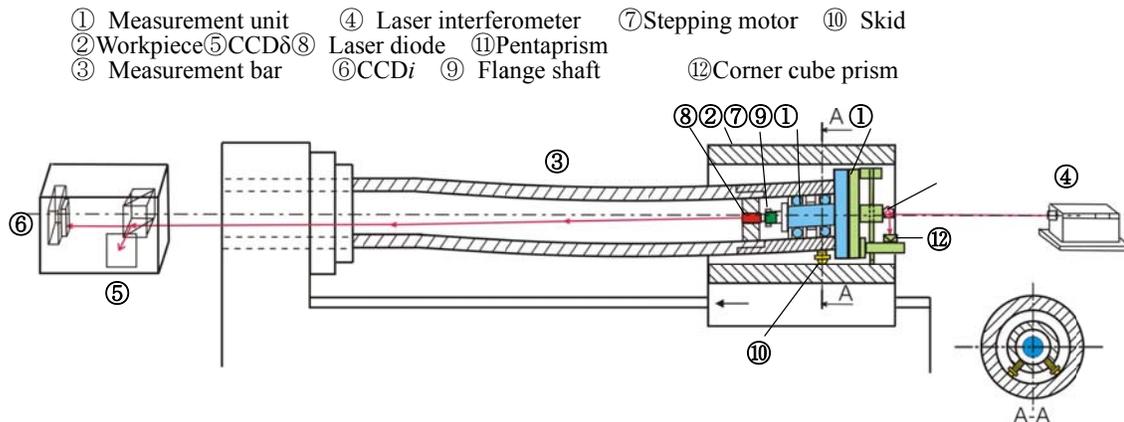


Fig.4: Laser-guided deep-hole measurement system without actuators

is placed in front of the measurement unit, via pentaprism [11] and corner cube prism [12], which are attached to the measurement unit.

A laser diode [8] is located at the front end of the measurement bar in order to detect the attitude (position and inclination) of the measurement unit. A laser beam passes through the measurement bar and reaches optical devices [5] and [6] to detect the attitude of the measurement unit.

In this measurement system, the laser diode is placed on the measurement axis, which is the center line of the spindle of the headstock, so the attitude of the measurement unit can be accurately detected. On the other hand, in the measurement system described in [1,3], a laser diode is fixed on the measurement probe apart from the measurement axis as shown in

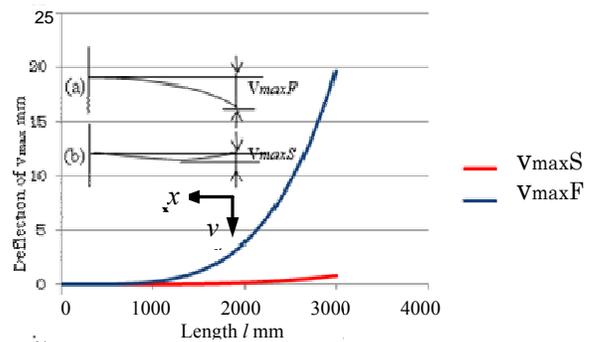


Fig.5: Maximum deflections of measurement bar

diode due to the rolling of the measurement probe affects the detection accuracy of the probe's attitude [4].

## 2.2 Relationship between Measurement Bar- Length and its Deflection

Figure 5 shows the relationship between the overhang length of a cantilever and its maximum deflection [4]. The beam has the following characteristics: steel material, Young's modulus  $E$  is 2.05 GPa, and the outside and inner diameters are 50 mm and 24 mm, respectively. Figure 6 shows the relationships between overhang length and inclination of the free end of the beam [5].

The following two conditions are illustrated: (a) is a cantilever with a free end, and (b) is a beam with a supported end.

(a) In the case of a cantilever with a free end

$$\text{---} \quad (1)$$

$$\text{---} \quad (2)$$

(b) With a supported end

$$\text{---} \quad (3)$$

$$\text{---} \quad (4)$$

where  $E$  is Young's modulus,  $I$  is the geometrical moment of inertia, and  $l$  is the length of the beam. When the length of the overhang is 3 m, maximum deflections are 19.66 mm and 0.85 mm in cases (a) and (b), respectively. In the case of (b), the maximum deflection of the beam occurs at 1.2645 m from the supported end. In this case, it should be noted that the hole wall does not block the laser beam at that position. At the end of the measurement bar, deflection  $v$  does not occur owing to support. Inclination angles  $i$  are  $-0.0087$  and  $0.00109$  in cases (a) and (b), respectively.

## 3. FACTORS THAT AFFECT MEASUREMENT ACCURACY

Problems that occur during deep-hole measurement are solved analytically and discussed below.

### 3.1 Inclination of the Measurement Unit

Section 2.2 shows the inclination angle at the supported end of a 3 m measurement bar.

Figure 7 shows the measurement parameters for deep-hole wall scanning. Sections AB and CD are the results of scans under normal and inclined conditions, respectively. If the hole wall is scanned when the measurement unit is inclined, the shape of the scanned hole is an oval. However, the data acquired by a laser interferometer indicates a circular shape even though the measurement unit inclines. The laser path between the laser interferometer and the corner cube prism does not change when the inclination angle is small [2].

When the diameter of the reference hole is

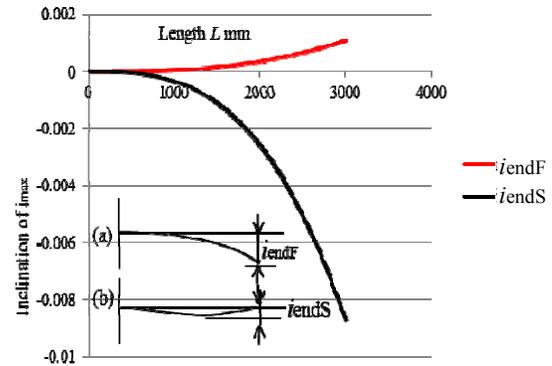
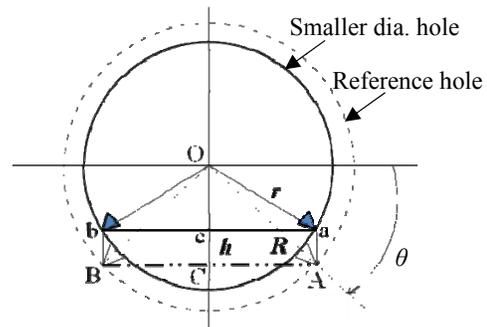


Fig.6: Inclinations at the end of a measurement bar

$$d = e \cos \theta$$

Fig.7: Influence of measurement unit inclination on measurement accuracy



A, B: Skid positions on reference hole  
a, b: Skid positions after sliding up on wall of smaller diameter hole

Fig.8: Two skids positions when entering small hole

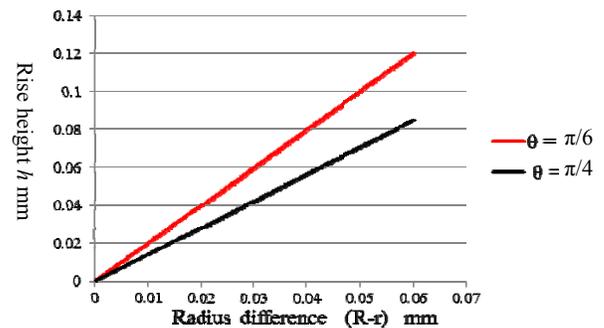


Fig.9: Relationship between skid rise and radius difference when entering small hole

$2R=63\text{mm}$ , the length of the longer axis of the oval is longer by  $0.037 \mu\text{m}$  than diameter of the reference hole. The longitudinal shift  $\delta Z$  of the scanning location is This longitudinal shift does not affect the accuracy of the hole measurement.

### 3.2 Effect of Changing the Hole Size

Figure 8 shows that skids A and B slide up on the wall of a hole with a diameter less than that of the reference hole.  $R$  and  $r$  are the radii of reference and smaller diameter holes, respectively.  $R=31.5 \text{ mm}$ ,  $h$  is the height difference of the measurement unit when skids A and B slide up on the wall of a hole with a smaller diameter than the reference hole. From the Pythagorean theorem for a right triangle, Eq. (5) can be obtained.

$$(5)$$

Figure 9 shows the relationship between radius difference ( $R-r$ ) and height of rise  $h$ , which is obtained from Eq. (3). The relationship is obtained when the position angles  $\theta$  are  $\pi/6$  and  $\pi/4$  rad. When the radius difference is  $0.06 \text{ mm}$ , the skid rises are  $0.12 \text{ mm}$  and  $0.085 \text{ mm}$  at skid positions of  $\pi/6$  and  $\pi/4$ , respectively. However, these values can be corrected using acquired data through an optical device for detecting the attitude of the measurement unit behind the headstock (Figs. 2 and 3).

## 4. GUIDELINES FOR A SIMULATION EXPERIMENT

It is very difficult to carry out an experiment using a measurement bar with outer and inner diameters of  $50$  and  $24 \text{ mm}$ , and a length of more than  $3 \text{ m}$  in the laboratory. In this experiment, the workpiece length, as well as the longitudinal feeding length, is  $3 \text{ m}$ . The total length of the machine becomes  $7$  to  $8 \text{ m}$  when the headstock length is included. In order to carry out similar measurement experiment for a bar with a diameter of  $50 \text{ mm}$  and a length of  $3 \text{ m}$ , a measurement bar with a diameter of  $18 \text{ mm}$  is taken into consideration, because a bar with this diameter is easier to bend than one with a diameter of  $50 \text{ mm}$ .

### 4.1 Calculation of Inclination Angle

Figure 10 shows a cantilever with a support at its end. At the location of  $0.5785l$  from the fixed end, weight  $P$  is loaded. In these conditions, the inclination angle  $i$  of the free end and supporting force  $R$  on the free end are written as:

$$R = \frac{3P}{3 + a} + 3w \quad (6)$$

$$R = \frac{4P}{3 + a} + 3w \quad (7)$$

Using Eqs. (6) and (7), measurement bar length  $l$  is determined under the condition that the slope angle  $i$  remains constant at  $0.00109$ . Outer and inner diameters of the measurement bar are  $18 \text{ mm}$  and  $12 \text{ mm}$ ,

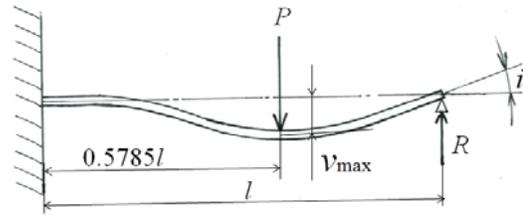


Fig.10: Cantilever with a support at free end.

respectively. The inclination angle at the end of the

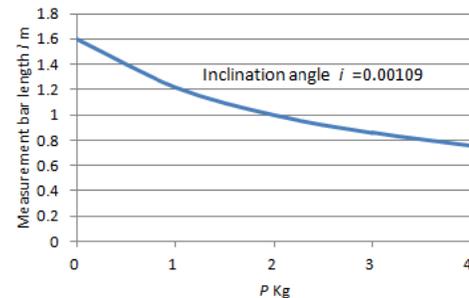


Fig.11: Relationship between load  $P$  and measurement bar length  $l$

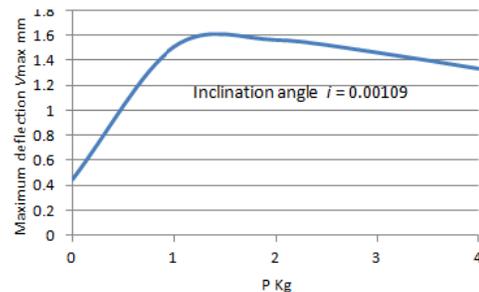


Fig.12: Relationship between load  $P$  and measurement bar deflection  $v_{\text{max}}$

measurement bar with outer and inner diameters of  $50$

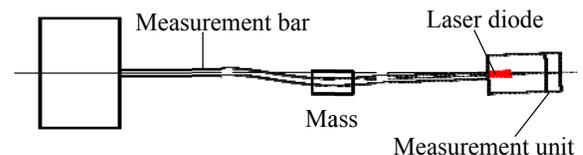


Fig.13: Simplified simulation model

and  $24 \text{ mm}$ , respectively, and length of  $3 \text{ m}$  is  $0.00109$ . The end of the measurement is supported.

### 4.2 Determination of Load

Figure 11 shows the relationship between the length  $l$  of the measurement bar and the load  $P$ . The length of the measurement bar for obtaining inclination angle  $i$

(0.00109) at the supported end decreases exponentially as the load  $P$  increases. Figure 12 shows the relationship between the maximum deflection of a boring bar and the load  $P$ . When a 1 kg mass is loaded, the length and maximum deflection of the measurement bar are 1220 mm and 1.5 mm, respectively. Under these measurement bar conditions, a simulation experiment using a lathe is easily carried out.

#### 4.3 Apparatus for a Simulation Experiment

The load  $P$  is applied by attaching a mass to the measurement bar. A laser diode is fixed in the measurement probe (Fig.13). The measurement probe consists mainly of a measurement unit, stepping motor, and laser diode. The hollow, slender measurement bar is also connected to the probe.

### 5. COMPARISON WITH LASER-GUIDED PROBE

A laser-guided deep-hole measurement system is particularly effective in cases where the hole length is quite large (Figs. 1 and 3(c)). The probe is always kept on the measurement axis by using six piezoelectric actuators, even though the hole diameter varies along the length of the hole. The probe's attitude is constantly monitored by the probe attitude detector and controlled so that the probe always remains on the measurement axis. In this case, high measurement accuracy levels can be obtained but the fabrication cost is very high.

On the contrary, the present probe is inexpensive to fabricate. By compensating using acquired data, accurate measurement can be obtained.

### 6. CONCLUSION

The accuracy of deep-hole measurements is discussed for the region where the bending rigidity of a measurement bar is low and the effects on measurement are easily compensated. The following results are obtained.

1. The developed system can measure the accuracy of a hole with a length of 3 m and diameter of 63 mm.
2. The effect of the changing attitude of the measurement unit on measuring accuracy is explained.
3. A method is presented for performing a simulation experiment by applying a load and using a small measurement bar with outer and inner diameters of 18 mm and 12 mm, respectively.

In the future, we will focus on the implementation of this method for measuring the accuracy of a deep hole a few meters in length through simulation.

### 7. ACKNOWLEDGEMENT

We thank Mr. H. Nakayama, an undergraduate student, for his cooperation.

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